

Section 4

PUMPS

4.1 GENERAL

Pumps add energy to a fluid. This energy can move the fluid through pipe and equipment, elevate the fluid, or increase its pressure and velocity.

Pumps are rated as follows:

- Capacity - the quantity of fluid discharged per unit time (gallon per minute)
- Increase in Pressure - frequently reported as head (feet of the fluid)
- Power - the energy consumed by the machine (horsepower)
- Efficiency - ratio of energy supplied to the fluid, divided by energy supplied to the pump (percent)

4.2 TYPES

We can classify pumps as centrifugal or positive displacement.

4. 2. 1 Centrifugal Pumps

Perhaps 90 percent or more of the pumps in process industries are centrifugal. This is because their design allows such great flexibility in flow rates, pressure ranges, etc.

Centrifugal pumps convert rotary energy into liquid pressure by a spinning impeller inside a casing. These pumps are usually driven by electric motors or steam turbines. Most centrifugal pumps have only one impeller or are single staged. However, if high pressure difference is required, multistage designs are used. We can mount centrifugal pumps either horizontally or vertically to suit the process.

Figures 4-1 through 4-10 are outline and cross-section drawings, showing design features of centrifugal pumps.

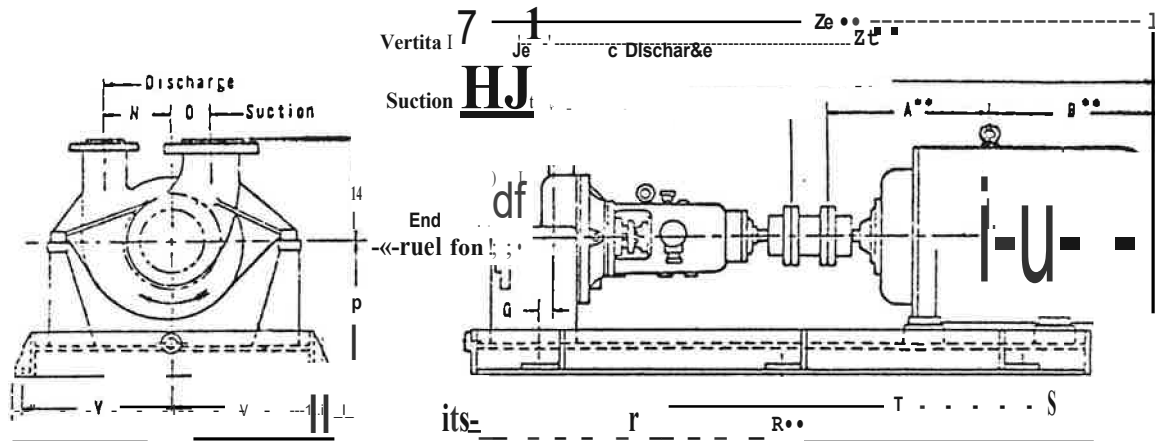
4. 2. 2 Positive Displacement Pumps

Positive displacement pumps are used to inject additives in very small amounts into main product streams, to transfer viscous liquids, and to pump quantities which are too small for centrifugal pumps. Figures 4-11 and 4-12 show reciprocating pumps, and Figure 4-13 shows nine classes of rotary pumps.

Positive displacement pumps trap a quantity of fluid in a chamber which is alternately filled from inlet and emptied through dis-

OUTLINE DIMENSIONS TYPE-CAD

Ser111 2.02 • 01
CAD DIMENSIONS
Januarr 31, IS64



Ze, Zt, A, B & R vary with driver - - Dimensions shown are for highest horsepower motor and stock base size.

All pumps listed with one size case except 4 x 6 x 13 which is furnished with two size cases (L) and (H).

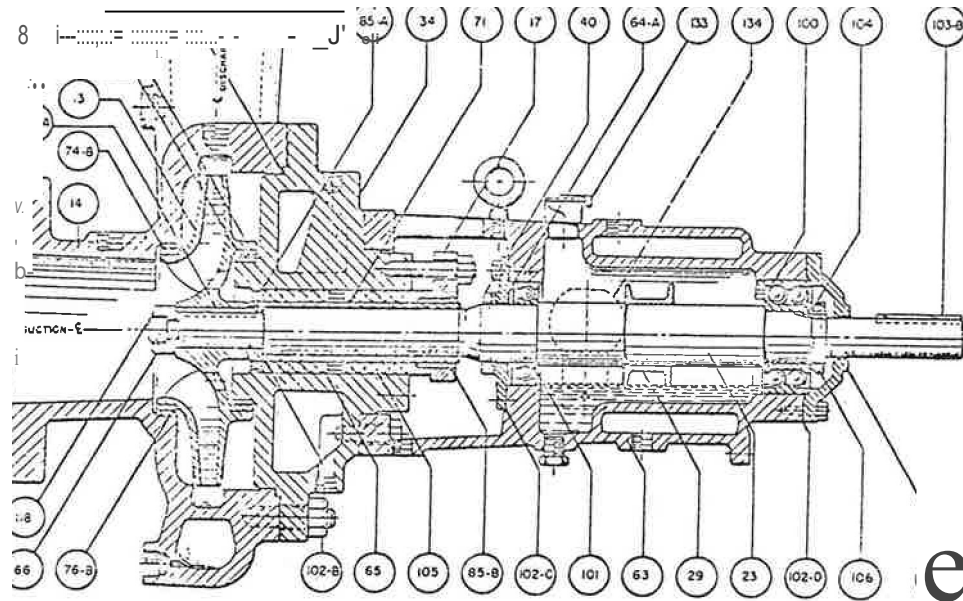
All dimensions are in inches. Do not use for construction unless certified.

Applies to Standard 300 ASA Raised Face Flange Only

Applies to Standard 300 - A3A - Raised Race F - Range Only																		
Size Dia., S-uc. b np s	Brg Prk1	ArD	Je	Jt	K	L	N	O	P	Q	R	S	S-IQ	T	ZV	W	Z	Zt
1 xi 1/2 x 6 1/4	24 5/8	5	11 1/2	23 1/4	4 3/8	7 3 1/4	2 1/2	13 1/4	1/4	56 1/2	6 1/4	6 1/2	6 1/2	30	27 1/2	31 1/4	53 3/4	
1 1/2x2x61/4	30	5	1 1/2	B 1/4	4 3/8	7 4		13 1/4	1/4	60 1/4	6 1/4	6 1/2	6 1/2	30	31 1/2	65 1/4	51 1/8	
2x3x61/4	7	3 11 1/2	6	2	23 1/4	4 3/8	8 4 1/2		13 1/4	1 1/4	60 1/4	6 1/4	7 1/2	30	31 1/2	65 1/4	51 1/8	
3x4x61/4		33 1/2	7	2 1/2	23 1/4	4 3/8	8 5		15 1/4	2 1/2	60	6 1/4	8 3/4	32	33 1/2	67 3/8	52 7/8	
11/2x2x81/2	30 1/8	2	2	27 3/8	4 3/8	9 5 1/4	3 1/2	17 1/4		72 1/4	6 1/4	7 1/4	7 1/4	32	33 1/2	89 1/4	65 1/8	
Zx3x81/2	37 1/2	6	2 1/2	27 3/8	4 3/8	10 5 1/2	3 1/2	17 1/4		72 1/4	6 1/4	7 1/4	7 1/4	35	36 1/2	75 1/4	71 3/4	
3x4x61/2	39 1/2	7	3	27 3/8	4 3/8	10 5 1/2	3 1/2	17 1/4		72 1/4	6 1/4	7 1/4	7 1/4	35	36 1/2	75 1/4	71 3/4	
4x6x6J/2	43 3/8	8	4	27 1/8	4 3/8	13 7	6 1/4	18 3/4	5/8	81 1/4	6 1/4	11 3/8	11 3/8	34 3/8	35 1/2	36 1/2	83 7/8	79 1/8
1 1/2x2x101/2	34	2	2	27 1/8	7 3/8	10 6	2 1/2	15 1/8	3/8	60	6 1/4	0 7/8	0 7/8	32	33 1/2	83 1/4	83 3/4	
2x3x101/2	49 3/4	7	2 1/2	27 1/8	4 3/8	10 6 1/2	4	18 1/4	2 1/2	90 1/4	6 1/4	8 3/4	8 3/4	39 1/8	35 1/4	33 1/2	88 1/4	
3x4x101/2	9 3/4	7	3	27 1/8	4 3/8	10 6 1/2	4	18 1/4	2 1/2	90 1/4	6 1/4	8 3/4	8 3/4	39 1/8	35 1/4	33 1/2	88 1/4	
4x6x10 1/2	52 3/4	8	11	30 1/2	11 1/2	12 7 1/4	6 1/2	22 1/2	5 3/8	107 1/4	6 1/2	12 1/4	12 1/4	45 1/8	43 1/2	106 1/4	104 1/4	
6x8x101/2	39 1/2	9	12	31 1/2	12 1/2	12 7 1/4	6 1/2	22 1/2	5 3/8	107 1/4	6 1/2	12 1/4	12 1/4	45 1/8	43 1/2	106 1/4	104 1/4	
1 1/2 x 3 x 11 1/2	9 3/4	7	2 1/2	30 3/4	11 1/2	12 7 1/4	6 1/2	22 1/2	5 3/8	107 1/4	6 1/2	12 1/4	12 1/4	45 1/8	43 1/2	106 1/4	104 1/4	
2 x 3 x 13	12 3/4	7	3	30 3/4	11 1/2	12 7 1/4	6 1/2	22 1/2	5 3/8	107 1/4	6 1/2	12 1/4	12 1/4	45 1/8	43 1/2	106 1/4	104 1/4	
3 x 4 x 13	10 1/4	8	3	30 3/4	11 1/2	12 7 1/4	6 1/2	22 1/2	5 3/8	107 1/4	6 1/2	12 1/4	12 1/4	45 1/8	43 1/2	106 1/4	104 1/4	
1 A x 6 x 13	9 1/4	6	4	30 13/16	11 1/2	12 7 1/4	6 1/2	22 1/2	5 3/8	107 1/4	6 1/2	12 1/4	12 1/4	45 1/8	43 1/2	106 1/4	104 1/4	
6 x 8 x 11 1/2	9 1/4	11	15	34	14	14 9	5	25	7 3/8	107 1/4	6 1/2	13 3/8	13 3/8	47 3/8	45 1/2	117 1/8	112 1/8	
3 x 4 x 14	59 1/4	9	3	33 3/4	6	14 8	5 1/2	25	3 1/8	107 1/4	6 1/2	13 3/8	13 3/8	47 3/8	45 1/2	117 1/8	112 1/8	
4 x 5 x 14	19 3/4	11	15	34 1/4	6	14 11	7	25	7 3/8	107 1/4	6 1/2	13 3/8	13 3/8	47 3/8	45 1/2	117 1/8	112 1/8	
6x6x14	19 3/4	11	15	34 1/4	6	14 11	7	25	7 3/8	107 1/4	6 1/2	13 3/8	13 3/8	47 3/8	45 1/2	117 1/8	112 1/8	
4 x 6 x 14	59 1/4	9	3	33 3/4	6	14 8	5 1/2	25	3 1/8	107 1/4	6 1/2	13 3/8	13 3/8	47 3/8	45 1/2	117 1/8	112 1/8	

Figure 4-1. Single Stage Horizontal Process Pump - End Suction.

BINGHAM TYPE CAD
PROCESS **PUWP** - ENO SUCTION



D AW/NG NO. WP-131

P. RT Hil.	OES IPTIOH	rUT H.C.	HS-RIPTIOH	PH H0.	OEHIPTTION
13	l r izIi er	66	Lockcol lar-tmpel lar	102-8	Gasket-Shaft Steiva
14	YeIi.te Casi f.,	71	Shaft Sleeve	102-c	Gasket-Cover,Pu..p tr.d
17	GIar.d	74-A	Impeller Rini-Hub	102-0	Gaskat-Cover,Oriva End
23	Shaft	74-8	lm el ler Rini:-Eya	103-A	Key•l pel ler
23	Gi I Spcol	76-A	Casin, Ring-Hub	103-B	Key-Shaft Extansion
H	Stuffin;; 6ox	75-8	Cas i ng Rini;-Eya	104	Lockwashe r-Saar i ng
40	Odlector u:sc	65-A	Packin, ain,	105	Packinz
SJ	aaaring iiracket	S5-a	SpIitRing-GI and	106	Locknut-Bear in•
ii4-A	Cover-Sa rini nadial	100	Thrust Baa ring	118	Lockscrew-tr:;pel ler
6-4-B	Cover-Bearing Thrust	101	ilad i a I Bearinz	133	Oi I Inspection Covar
65	lantern Rln,	102-A	Gasket-Yo lute	134	Constant Leval Oil ar.

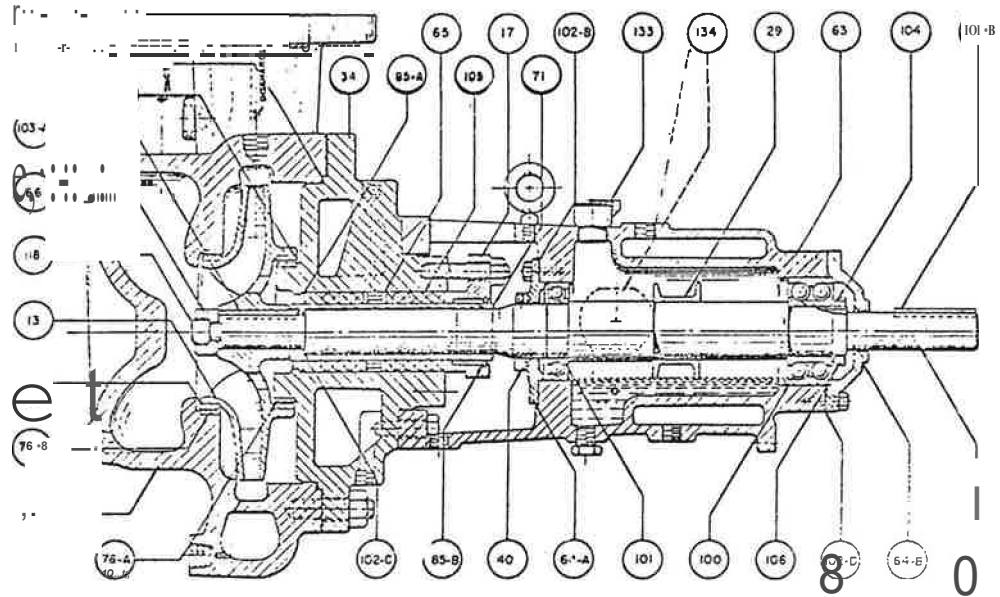
Sup1r,1d11 ZS-2551

----- :_i;ⁿ_j -1- c_i a_j l < 2 : , a_j T L - a_i , 11 . . . c . . c . . - c . . c . . a .

Figure 4-2. Single Stage Horizontal Process Pump - End Suction.

BINGHAM TYPE CAD

Small LOJ • (j)
CAD mss mr10K
uc" 20, 1111



DRAWING SG 2-130

R T H.O. I	DES CR I PT FOK	HO.	DESCRIPTION	PART NO.	ESC I IJh
1;	Impeller	66	Lock collar-Impeller	102-B	Gasket-Cover, bearing
14	Volute Casing	71	Shaft Sleeve	102-C	Gasket-Shaft Sleeve
17	Impeller	H-A	Impeller Ring-Hub	102-D	Gasket-Cover, bearing;
23	Shaft	H-B	Impeller Ring-Eye	103-A	Key-Journal
29	Diaphragm	76-A	Casing Ring-Hub	103-8	Key-Shaft Extension
34	Stuffing Box	76-B	Casing Ring-Eye	104	Lockwasher-bearing
40	Deflector Disc	85-A	Packing Ring	105	Packing
63	Sealing; bracket	85-8	Split Ring; Cland	106	Locknut-Bearing;
64-A	Cover-Bearing Radial	100	Thrust Bearing	11B	Lockscrew-Impeller
64-B	Cover-Sealing Thrust	101	Radial Bearing	133	Oil Inspection Cover
65	Lantern Ring	102-A	Gasket-Volute	1H	Constant Level Dial

Supersedes 2S-2185

Bingham FACTORIES: PORTLAND, ORE. VANCOUVER, B.C., CANADA

Figure 4-3. Single Stage Horizontal Process Pump - Top Suction.

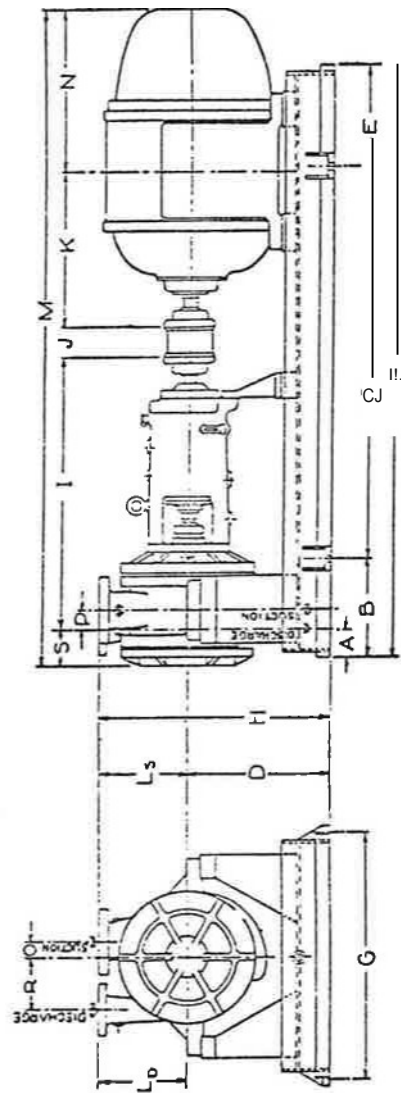
330-16 JUNE 57

Byron Jackson
mcl:m:0 Umps

su,uou ALL
mv.ous 111uu

HORIZONTAL MULTI-STAGE - SM PROCESS PUMPS 2 STAGE SM PROCESS PUMPS

OUTLINE DIMENSIONS



SIZE	Disch.	Suct.	I	J	L _D & L _S	O	P	R	S
1 1/2 x 2 1/2	1 1/2	2 1/2	3 1/2 - 7/8	4 - 3/8	9	1 - 1/4	2 - 1/4	5 - 3/4	3 - 11/16
2 x 3	2	3	4 - 1/2	5 - 1/8	12	1 1/2	3 1/2	6 1/2	4 - 1/4
2 1/2 x 4	2 1/2	4	5 - 1/2	6 - 1/8	15	2	4 - 7/8	7 1/2	4 - 1/8
3 x 4 1/2	3	4 1/2	6 - 1/2	7 - 1/8	18	2 1/2	5 - 7/8	8 1/2	6 - 1/8
4 x 6	4	6	7 - 1/2	8 - 1/8	21	3	6 - 7/8	9 1/2	4 - 1/4

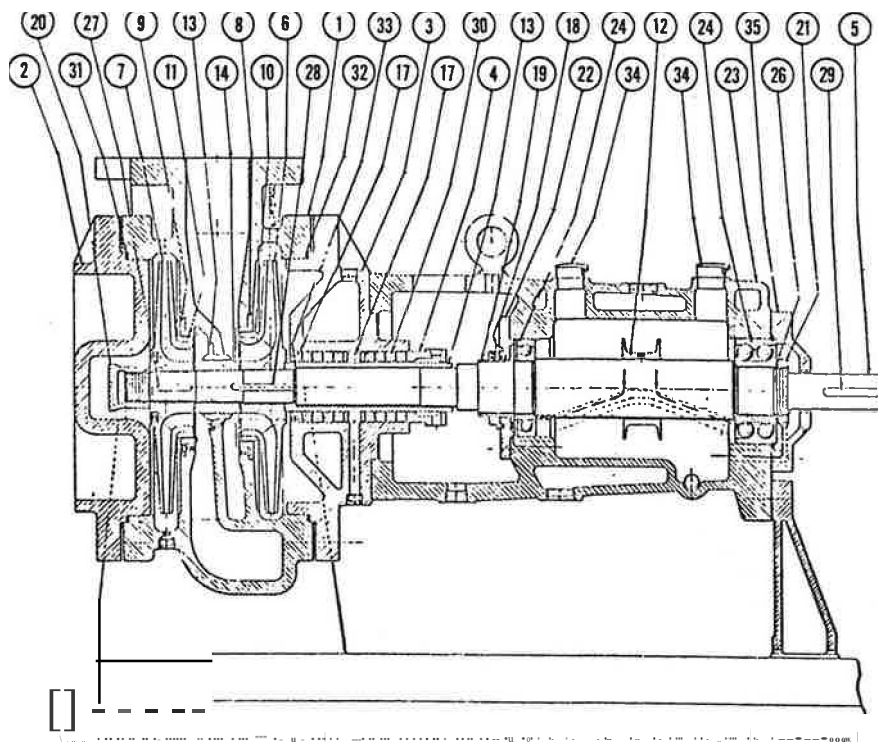
All Dimensions Are In Inches & Are Approximate
Used For Construction Purposes.
Dimensions Not Given Depend On Driver Us



Drawing No. 28-8441
QUALITY PUMPS SINCE 1872

Figure 4-4. TwoStage Horizontal Process Pump.

11-1



PART NO.	NAME OF PART
2	PUMP CASE
3	PUMP COVER - OUTBOARD
4	PUMP COVER
5	GLAND
6	SHAFT
7	IMPELLER - 1st STAGE
8	IMPELLER - 2nd STAGE
9	IMPELLER WEAR RING - 1st STAGE
10	IMPELLER WEAR RING - 2nd STAGE
11	CASE WEAR RING - 1st STAGE
12	CASE WEAR RING - 2nd STAGE
13	OIL FLINGER
14	SHAFT SLEEVE
15	IMPELLER SPACER SLEEVE
16	CENTER BUSHING
17	THROAT BUSHING
18	GAGE RING
19	DEFLECTOR
20	DEFLECTOR SLEEVE
21	IMPELLER NUT
22	THRUST BEARING NUT
23	BEARING COVER - INSIDE
24	BRACKET
25	BALL BEARING - THRUST
26	BALL BEARING - RADIAL
27	BEARING LOCK
28	IMPELLER KEY - 2nd STAGE
29	IMPELLER KEY - 1st STAGE
30	COUPLING KEY
31	PACKING
32	GASKET - CASE & COVER
33	GASKET - PUMP CASE g. COVER
34	GASKET - SHAFT SLEEVE
35	OIL FILLER CUP
	BEARING COVER - COUPLING END

WHEN ORDERING PARTS REFER TO
DWG. NO. IF 17121 AND TO PART NO.

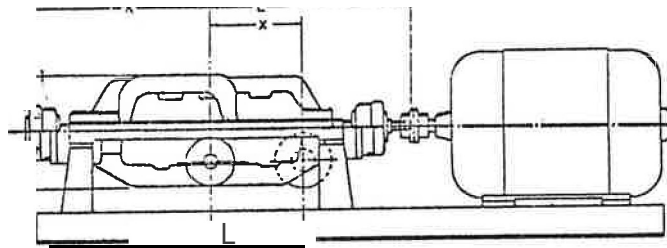
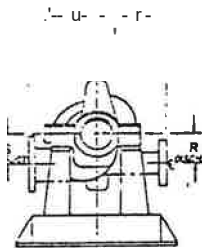
<-WHEN GLAND IS BUSHED
ORDER PART NO. 113
GLAND BUSHING

Figure 4-5. Two Stage Horizontal Process Pump.

IM RTAHT
F.P., -100 111 1111,0111111

OUTLINE DIMENSIONS TYPE MSB STYLED SINGLE SUCTION - nouALE VOLUTE PUMPS

MSB-D DIMENSIONS
L"tr Lie 111



Ty: ■ MSI-0 puops • r n all bll • ii ■ h r clodwiu (CD) or counl rre lack lu (CCD) rau llan, u vined frao lh colliplini •nd, u:d ,n) lyPt ol ■ator , aur. turbine or Inclnl drivl. r,U di,urlllonl bllaw trl lar ball bu ina puapo ol ER ralalion, Wini ,u ■ 11,n., rmlnl en noult 11;11111 allnl - 3001 AU, cul Iron cuina - z50, AU.

All di.. naion, ■ r ■ In inchu and fir luldlncl inly, C111111d druIn11 1111 b ■ provl dmd In 111 0111 al actual 111111ructlan.

Size	Number Stages	G	H	K	L	R&S	T	U	X
3 X , X g	4	12	12	25 1/2	31 5/1	6.1i	14	14	12
	5			29 1/2	35 ua				15
	6			33 1/2	39 5/1				g
	7			37 1/2	43 5/8				2
	8			41 1/2	47 5/1				2'
	9								
	10								
	11								
3 X 6 I 10 1 X 6 X 10	5	13	13	27 1/2	H 1/4	7	15	15	1 ...
	5			32	38 3/4				19 1/2
	7			36 1/2	43 i,1				H i,1
	8			4i	47 3/4				27
	9			45 1/2	52 1/4				31 3/4
	10								
	11								
	12								
4 X 6 X 10!11		14 1/1	14 3/8	26 11,	35 3/8	8	17	17	1 ,n
				11	40 1/1				lg 11 ,
	7			37 31,	44 7/8				H
	8			42 1/2	50 5/8				2; J/4
	9								
	10								

Superseded April 15, 1953

Di:111/ NGNO. -n P- 182



Figure 4-8. Horizontal Split Case Multi-Stage Pump.

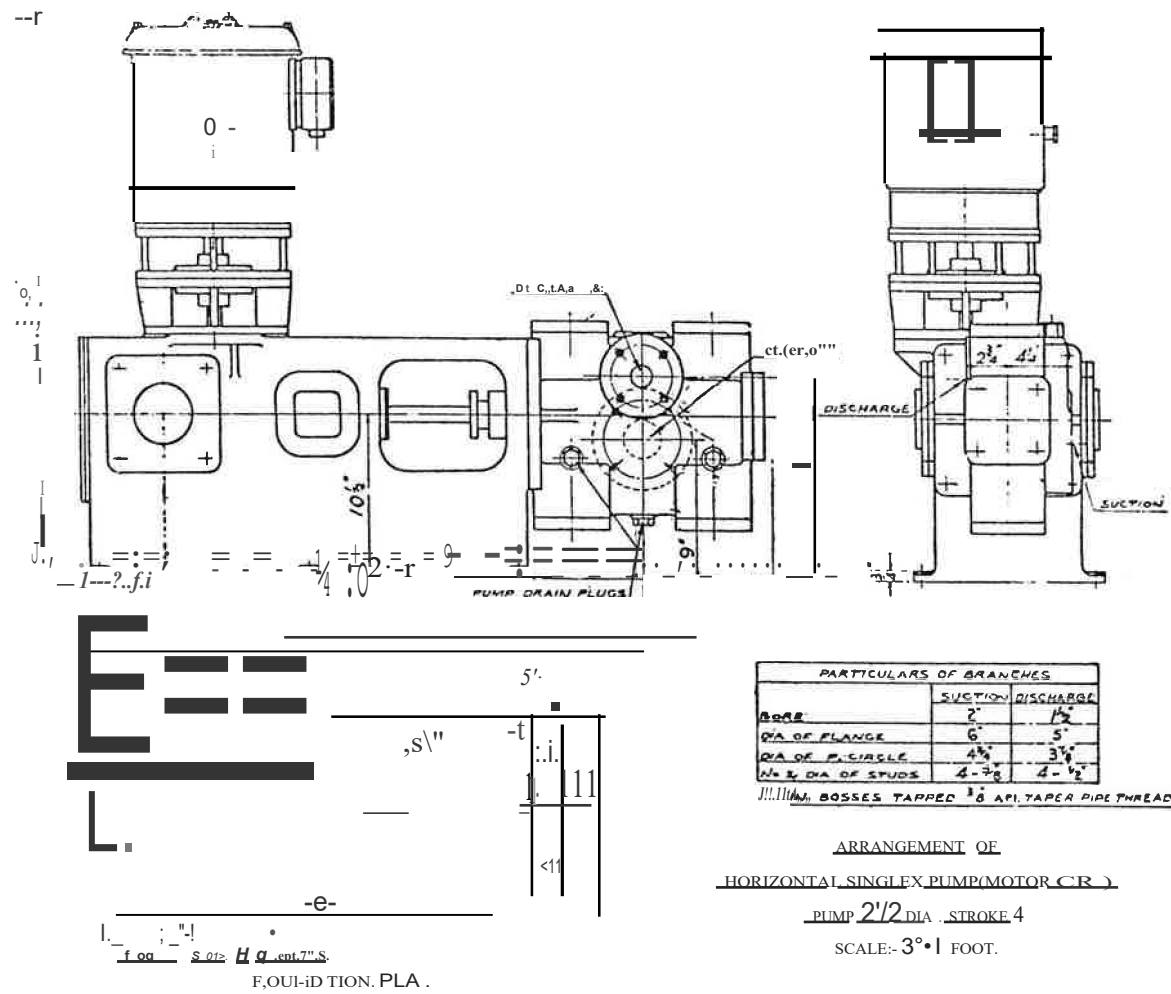
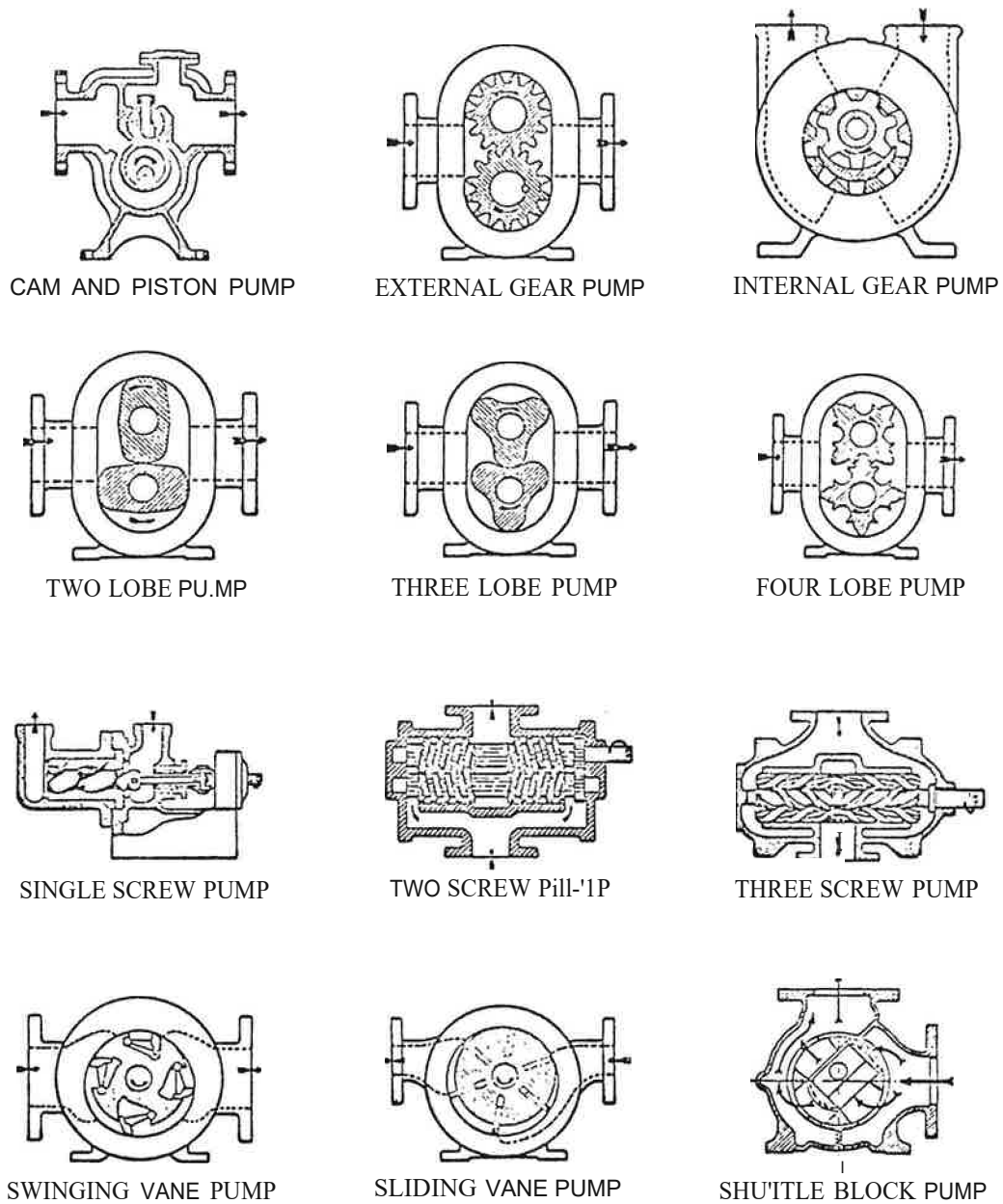


Figure 4-11. Horizontal Singlex Pump.



A rotary pump is a positive displacement pump, consisting of a fixed casing containing gears, cams, screws, vanes, plungers or similar elements actuated by rotation of the drive shaft. These pumps are

characterized by their close running clearances and the absence of suction and discharge valves. Various types are shown by the cross-sectional drawings.

Figure 4-13. Classes of Rotary Pumps.

charge. These pumps do not allow free flow of fluid through the pump. Positive displacement pumps are either reciprocating or rotary. In reciprocating pumps, the fluid chamber is stationary; in rotary pumps, the chamber moves.

4-3 GENERAL PUMP INFORMATION

Certain features of pump design are of direct interest to the piping designer:

- Each pump will have connections termed "suction" and "delivery" or "discharge". These connections vary with the size of the pump and may be flanged or screwed to the required standard.
- Where cast iron is used as a casing material, flanged connections are flat-faced ASA 125 or 250 rating, and with steel or alloy castings they are raised-face ASA 150 or higher.
- Pump casings may have vent and drain connections to suit the customer. This may require special piping of vents and drains.
- Most baseplates, especially those for centrifugal pumps in hydrocarbon service, have drain rims to collect leakages from the pump. The drain rim has a tapped connection which is usually piped to a drain hub.

- Most centrifugal and positive displacement rotary pumps have mechanical seals. The pump maker usually supplies a mechanical seal harness. When the pumped fluid is used for seal circulation, piping is attached to the vent connection on the casing. The circulated seal fluid must be returned to the pumped stream and maybe piped back to the suction -or returned through the seal and pump internal clearances.
- When pumping viscous or high temperature hydrocarbon liquids, the seal fluid (usually clean gas oil) circulates from an external source through connections on the pump seal.
- Double mechanical seals have inlet and outlet connections for seal fluid circulation.
- External seal oil piping appears on the P&ID.
- High temperature pumps usually need water cooling for stuffing boxes, bearings and pedestals supports. The pump outline drawing shows how much cooling water is needed, and the connections, points, and sizes for the inlet and outlet. Figure 4-14 shows a typical water cooling circuit.

Figure 4-15, a pump data sheet, summarizes operating conditions, design limits and materials of construction.

FOR 7-*: J J' . REQUISITION NO i o j i c -
SITE L C; e UNIT J G ITEM NO Zr. 3T9t 26-370
SER: ICE k-/A IVVL * 57 f't c' ffH MOTOR DRIVE .. 2 TURBINE DRIVE ...
PUMP MFR (5 u i n d4) 0" 9xv- 4 SIZE AND TYPE 314 L14 NO. REQ'D G., 4 0
API STD. 610 APPLIES YES HO

[illegible]

MATERIAL I CODE-ENTER/ALIAS CASING		INTERNAL PARTS		SHOP TESTS REQUIRED		WTN:SSL 11
I -CAST IRON	NITE BLNCAOE	I B f s t c	X	RUNNING PERF	Yf	IVO
B - BRONZE	IMPELLER	I 9 s c	11. # E 11 /	NPSH	1.10	-
S - STEEL	INNER CASE PARTS	I I S C	S	HP (C) 1A	1.10	1.10
C - 11-13% 0-ROME	SLEEVE (PAC KED J	Ch Ch Af Af		HYDROSTATIC	PSIG	No
A - ALLOY	SLEEVE (SEAL)	C C G C	18	MAX ALLOW WP	100 PSIG	100 F
h - HARDENED	WEAR PARTS	I B ch Ch	1.5 E (	WEIGHTS	PUMP EFASE	755 #
f - FACER,	SHAFT	S s s g t S	\$			
X "		t				
MOTOR DRIVER BY		TURBINE DRIVER BY		MFR FINAL DATA		I\$ BUILT)
ITEM	HP ML RTR	ITEM NO	MTO BY	ACTUAL IMPELLER DIAM		
HP LS RPM	FRAME	HP	RPM MATI			
MFR		MFR and	TYPE	1ST CURVE NO		
TYPE	INSUL	INLET STE AM	psQ	TEMPF		
ENC	TEMP RISE C	E X HAUST		PUMP SECT OWG NO		
VOLTS/ PH/ SE/ CYCLES		STEAM RATE, FL	ft, BHP/HR	SEAL DIM DWG NO		
BEARINGS	LUBE	BEARINGS	LUBE			
FULL LOAD AMPS		NOZZLES I SIZE	LOSITO	PUMP SERIAL		
		UHAUST		No 2 6' 36 1		
				16-370		
				2.1-0484		

[illegible]

	2	6/2/65	REV. AFTER COMES, PERT, ADDED DATA	JRM	100		JOB NO	DRAWING NO	REV
	1	4/15/65	ISSUED FOR QUOTATION	JRM	TVB				
	3	2/25/65	ISSUED FOR QUOTATION	JRM	100		5099	DS-24-69	3
	4	1/27/65	ISSUED TO CARTEL	JRM	100		SHEET	1	OF

4-19

4. 4 PIPING

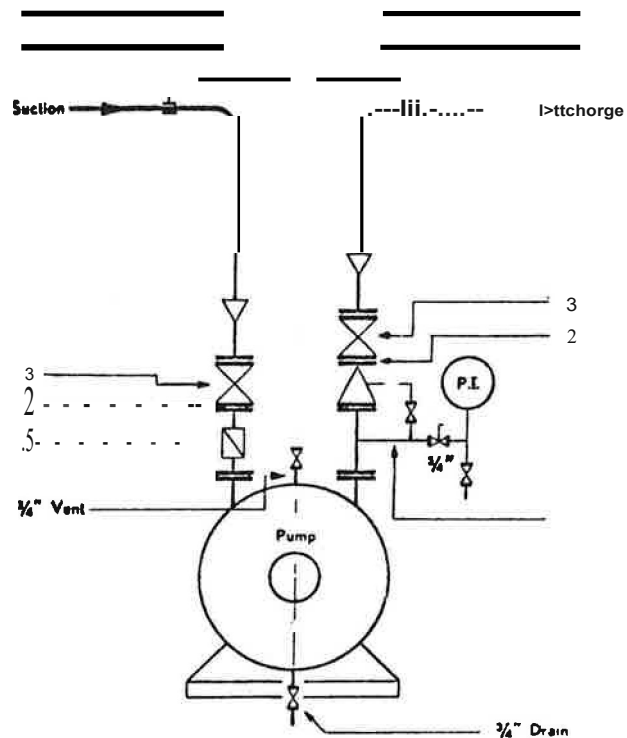
The piping designer should assist the engineer in selecting a pump so connections will suit the best piping hook-up. This includes choosing between such combinations as end suction - top discharge or top suction - top discharge, etc. The designer is in a good position to look into stress and expansion problems which develop when pumps are manifolded together. He can also check vendors' drawings and auxiliary piping drawings for vents, drains, cooling water to bearings, etc.

The pump outline drawing (supplied by the vendor) tells the piping designer the size, rating, and position of suction and discharge connections on the pump (Drawing 29-041-211). Figures 4-16, 4-17 and 4-18 show typical piping hook-ups for centrifugal and reciprocating process pumps. We can classify most piping at the pumps into suction and discharge lines. The two sections which follow list the important principles used in piping lines of this type. Although the engineer is responsible for most of these aspects, the piping designer should also check to see that they are fulfilled by the P&ID.

4. 4. 1 Suction

- Use a minimum of fittings such as bends and reducers
- Keep suction lines as short as possible

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NOTES,

Piping at pump, should be adequately supported so as to prevent any strain on the pump during operation and further to allow easy removal of the pump.

2 Spectacle blind, should be provided in piping if - rigid for installing slip blind.

3 Valve should normally be of the same size as the pump flange. However, the suction condition should be carefully checked.

• Pumps handling hot or high pour point liquid, should be equipped with 1/4" (minimum) by-pass around the check valve.

5 Temporary lift-up liners should be provided with projecting indentifying rib or handle.

CENTRIFUGAL PUMPS PIPING ARRANGEMENT FOR PROCESS PUMPS	
	January 1960
ROYAL DUTCH/SHELL GROUP	DE 31. 29. 02. SO - Cen.

Figure 4-16.

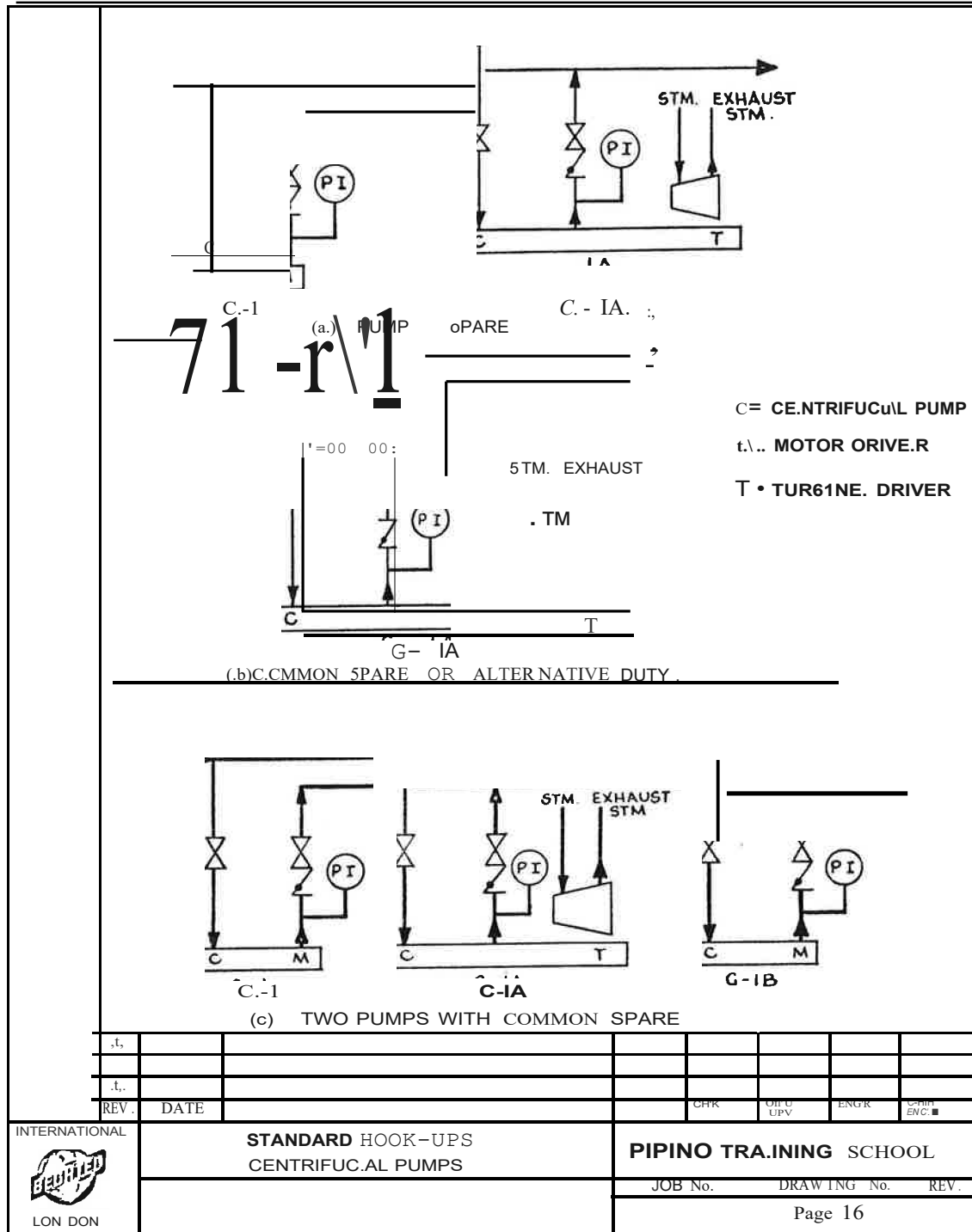


Figure 4-17.

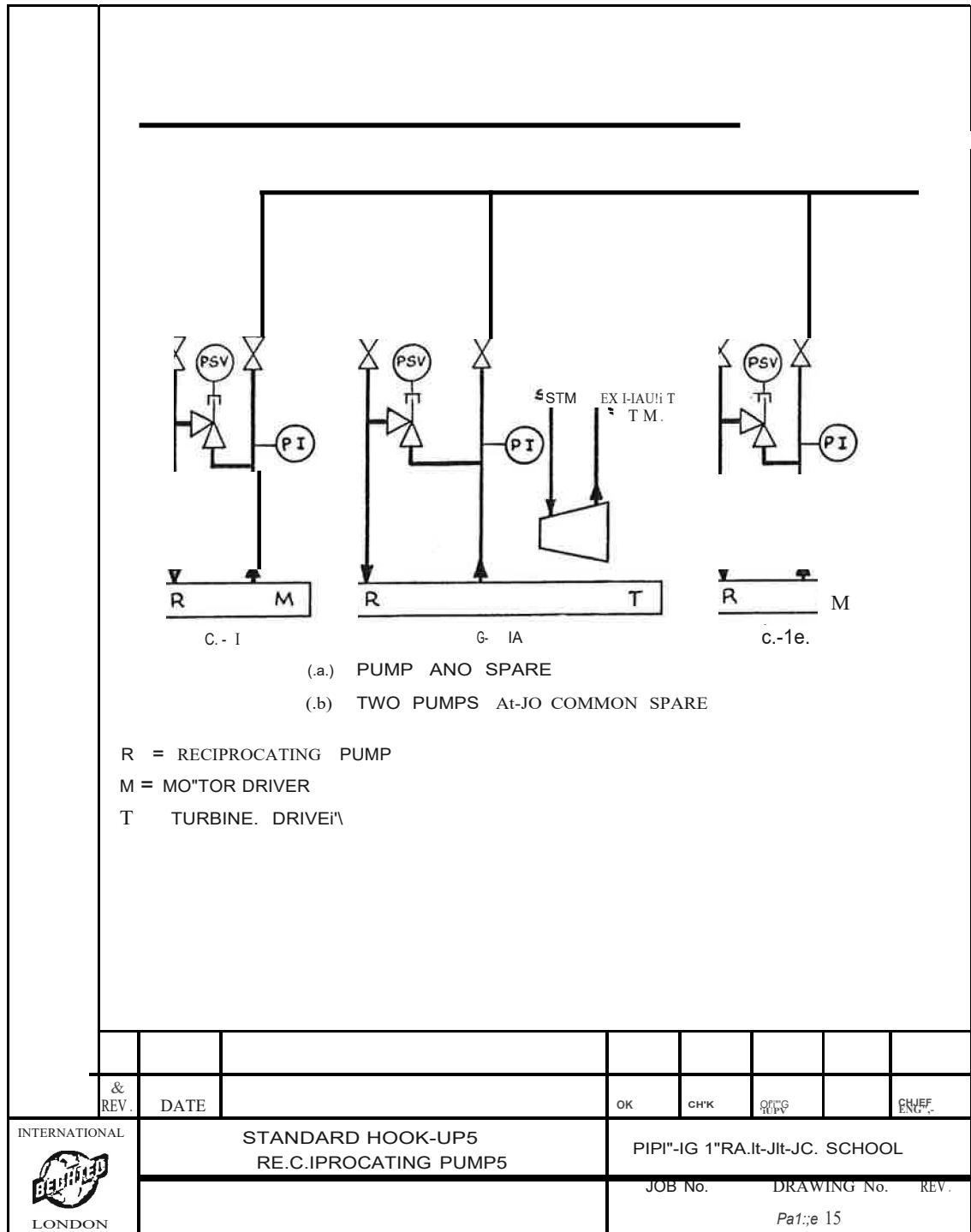
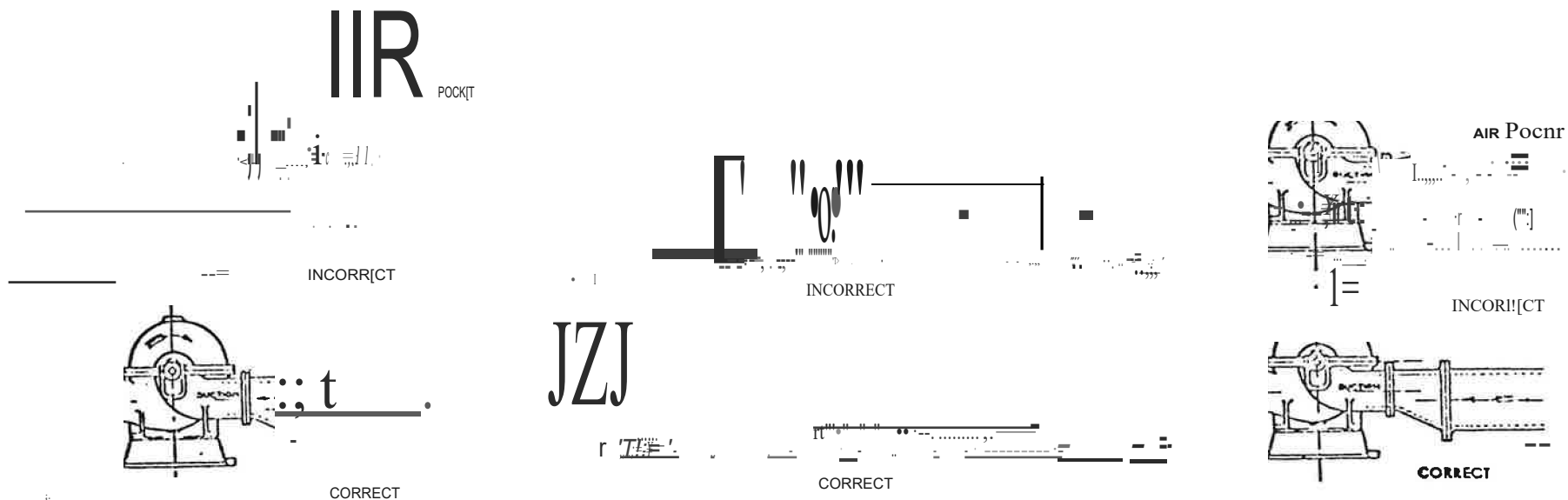


Figure 4-18.

- Check P&ID to see that the suction lines are not smaller than the pump nozzle .
- Don't allow pockets that can trap air
- Arrange eccentric reducers so they will release vapor bubbles . This usually means inverting the eccentric reducer (Figure 4-19)
- Provide temporary strainers in lines
- If possible, don't place an elbow horizontally at the suction nozzle of a centrifugal pump. If such an elbow is needed, place it at least three pipe diameters from the pump
- If you must use a right angle bend next to the suction nozzle of a double entry centrifugal pump, then install the bend vertically. This prevents an unbalanced flow to the impeller

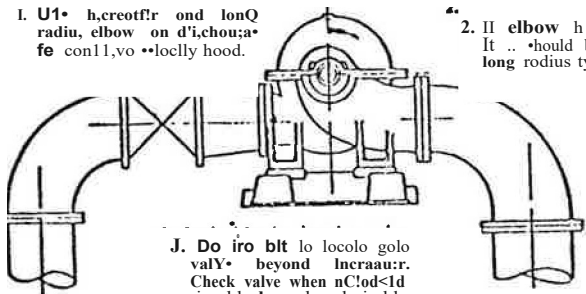
4.4.2 Discharge

- Provide an orifice on horizontal centrifugal pumps to by-pass some discharge at low flow rates
- Protect positive displacement pumps by a pressure relief valve that connects the discharge back to the suction. However, the pump may have a built-in safety valve
- Provide a check valve between a centrifugal pump and the shut-off valve. Locate a drain on the upstream side of the valve

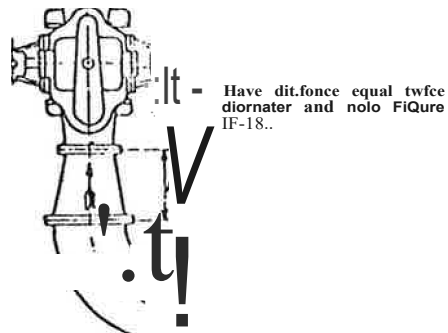


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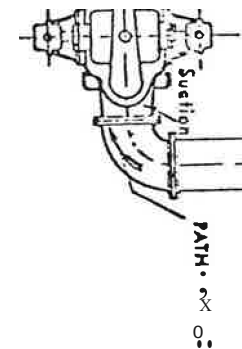


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Figure 4-19.

Cavitation Problems.

- Put a pressure gage on discharge lines upstream from the block valve

4.4.3 Valves and Auxiliary Piping

This section describes other important piping principles which aren't classified under suction and discharge. Again, the piping designer should check to see if the P&ID follows these principles:

- Arrange valves and piping so the maintenance crew can easily work on the pump, and so that other equipment doesn't have to be shut down
- Keep suction and discharge valve handwheels on a common center line above the operating floor
- Make block valves full line size, up to and including two inches. Above that size, if there's only one pipe size difference between pump nozzle and line, then the valve will be line size. If there are two or more size differences, then the valve may be one size less than line size
- Arrange and support piping to prevent strain on the pump from thermal stress or unsupported pipe
- Provide pumps handling liquids that might freeze with a casing drain. For other than freezing service, provide a drain valve between the block valve and pump suction

- Trace and jacket pumps handling liquids that may solidify
- Use a drain hub at all pumps. Connect all pump drips and vents to the pump bedplate or drain hub. Pipe all drains except those for solvents to the oily sewer
- Check the mechanical seal flushing system for inlet, outlet, drain, and vent connections

4.5 LAYOUT

4.5.1 Pumps

Pump piping has been a subject of considerable controversy.

Why? Basically, we have two conflicting schools of thought:

- (1) Isolate pump from piping, to provide maximum access for both in-place maintenance or removal.
- (2) Combine pump and piping in a compact area surrounded by well-defined walking areas free from hazards such as projecting valve stems.

Both of these concepts have obvious merit, but we cannot satisfy both completely. Again, we compromise.

However, before we examine the "ideal" pump layout (a hypothetical case tailored to illustrate just what we want it to), let's look at a few more basic considerations:

- (1) What kind of a pump do we want? Obviously, we will select a pump of a type which will perform in the service specified,

but once the process design conditions are satisfied, we will tend to base our choice on economic values.

An example: for a given service, we may be offered pumps with end, top or side suction. One, and only one of these choices will be ideal from the piping standpoint. However, when possible, we should select the most economical pump.

In general, the following suggestions (Table A) will provide some guidance to choice between end and top suction pumps, but individual situations involve so many variables (pump size, line size, valve size and type), that there is really no proper substitute for early consultation with the piping lead draftsman.

TABLE A

Small (up to 4" suction)	Elev. vessel	Top suction and discharge
Small (up to 4" suction)	Low vessel	End suction and top discharge
Medium (6 ¹¹ and 8 ¹¹)	Elev. vessel	Top suction and top discharge, if possible (check this with piping)
Medium (6 ¹¹ and 8 ¹¹)	Low vessel	End suction and top discharge
Large (10 ¹¹ and u.p)	Elev. or low vessel	End suction and top discharge

Side suction pumps will be a nuisance from the space standpoint in most *cases*, and should be avoided unless no other pump will satisfy the pumping conditions or in those rare cases (such as alongside a cooling tower basin) where side suction might be ideal. In the event that a side-connected pump of the double-suction type is selected, another problem appears: suction piping must be arranged so that one-half of the inlet flow is directed to each side of the impeller or reduced efficiency and improper loading of the pump bearings will result. This can be done in three ways:

- (a) High-suction source: suction line should drop vertically at the pump with the elbow at inlet in the vertical plane
- (b) Low-suction source where there is plenty of room: allow at least five diameters of straight pipe directly before the inlet
- (c.) Low-suction source where space is not available and an elbow in the horizontal plane must immediately precede the inlet: install a splitter vane in the elbow

Now, assuming we are dealing with a pump which is well selected for our particular situation, we can go on to the rest of our considerations.

(2) Ease of Access to Pump for Minor (in place) Maintenance:

- (a) Pump maintenance points are largely concentrated in the packing gland area. Auxiliary piping connections to coolant or seal fittings contain small valves and strainers which must also be accessible
- (b) Turbine drivers have similar maintenance points and auxiliary connections

(3) Ease of Removal of Pump or Driver for Shop Maintenance:

- (a) Small pumps are not much of a problem. Two men can lift them onto a hand truck, but adequate space must be left for the men and the truck
- (b) Medium size pumps will be handled by an A-frame or a motorized crane. Space must be left over the pumps for A-frame or crane boom with reasonable clearance for rigging. Eleven feet clearance above grade in the area around and over the pump is needed if a small crane of the "cherry-picker" variety is to be used. If such a crane will not be used, this clearance can be reduced, but should not be less than eight feet
- (c) Large pumps will definitely require a heavy duty crane. Overhead clearance must allow for the

size of the crane, the overall height of the pump and adjacent pumps, and space for the necessary rigging. In instances where a large crane cannot be positioned, monorail, gantry structure or in-place maintenance provisions might be considered.

- (4) **Positioning of Valves:** Locate valve handwheels in natural positions for ease of operation, but avoid creating hazards to personnel with protruding valve stems or head-knocking handwheels.
- (5) **Reasonable Support of Piping:** Pump flanges can normally support only small piping not subject to great expansion stress. Piping must be arranged so that suitable supports and anchors can be provided. This is part of the original design problem and should not be handled as an afterthought. If piping is to be supported from grade, then supports should rest on a slab which is integral with the pump foundation.

Now we are ready to pipe up a pump. We have selected a simple case and piped it in the worst possible manner (Figure 4-20).

With this simple example, which at a glance appears reasonable, we have managed to violate all of our basic concepts of good practice. Let us examine this arrangement in detail:

- (1) A top suction pump would have been a more suitable choice
- (2) Discharge piping interferes with in-place maintenance
- (3) Discharge cross-over line interferes with removal of pump
- (4) Suction valve is a hazard
- (5) Discharge valve is a hazard and *is* not conveniently placed for operation
- (6) Suction line is supported by removable suction spool
- (7) Discharge piping cannot be reasonably supported at all

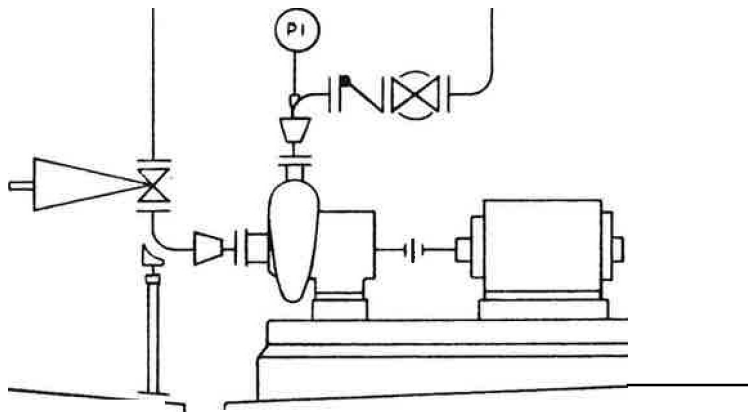
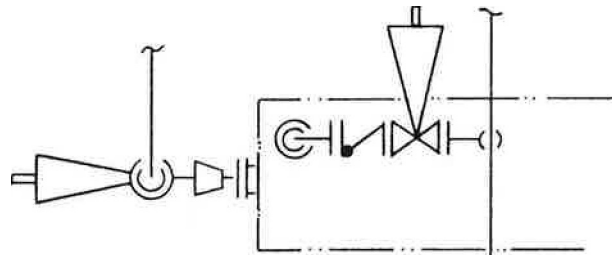


Figure 4-20.

As a bonus Figure 4-20 illustrates a few additional "honors".

(I) Valves should have been "pump size", not "line size"

(Z) Reducer (if not relocated in riser on other side of valve) on suction nozzle should have been eccentric to avoid line pocket

{3} Extra cost in unnecessary fittings

How should the pump in Figure 4-21 be piped? Let's assume that we are stuck with the same end-suction pump, and only the principles we have outlined;

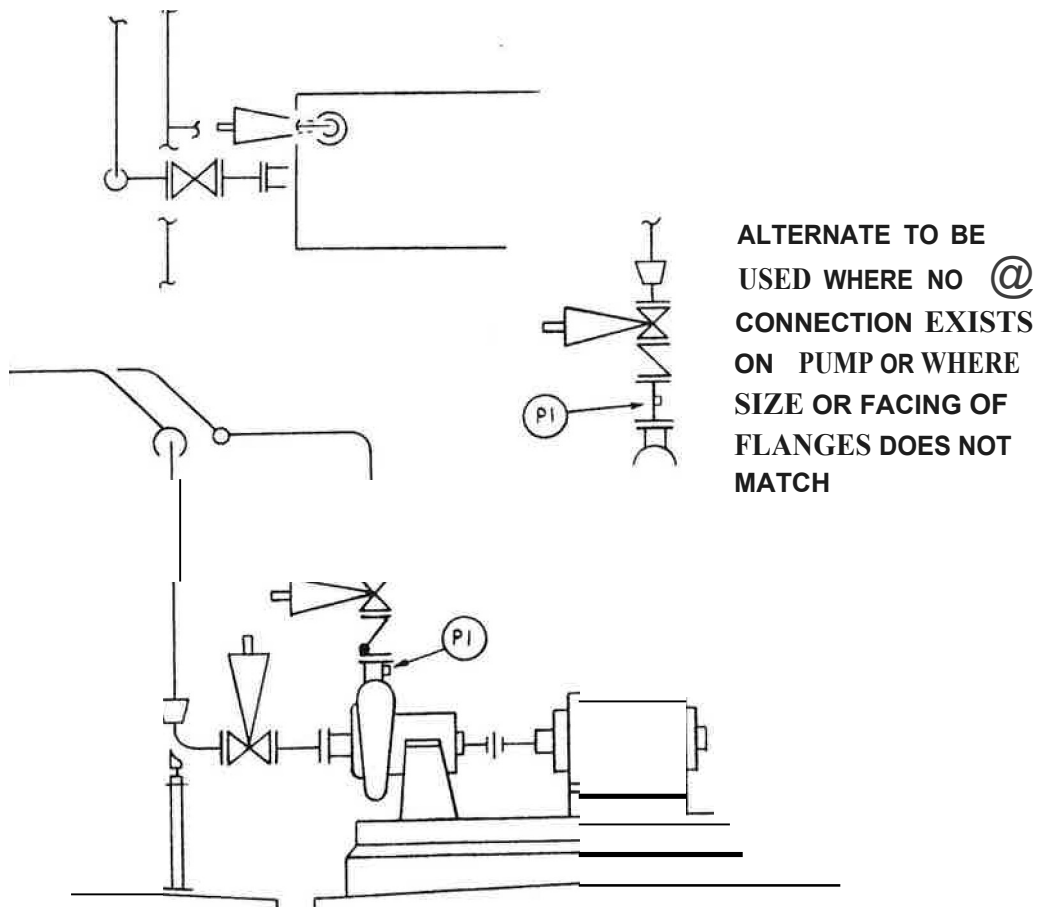


Figure 4-21.

Not only have most of the problems disappeared, but we have saved an appreciable amount of money through the use of fewer fittings and smaller valves.

The foregoing example demonstrates the one major rule to remember for fulfilling most of our basic requirements more easily:

"The general mass of piping, valves, and manifolding for a pump should be placed in a compact area in front of the pump. "

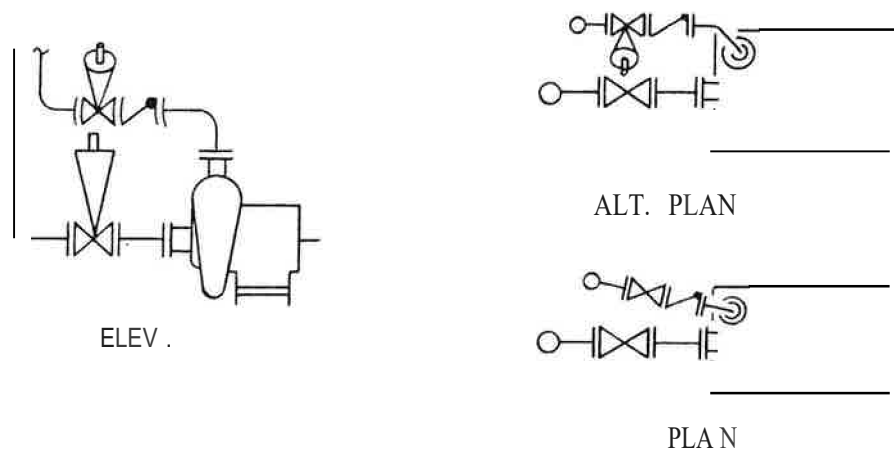
Most of our recent plant designs have recognized this as a fact, and space consistent with the size and complexity of the piping (usually about four feet) has been allotted for this purpose. Most of the poor arrangements of the past have resulted from failure to recognize this need. Consequently, piping was crowded over and around the pump.

Piping should enter and leave the pump with a minimum number of offsets. Discharge valves, for example, should always be placed in the riser above a top discharge nozzle unless one of the following conditions governs:

(I) Confined gasket facings are involved, and piping is so inflexible that gaskets or removable spools can not be extricated

(2) Pump and v.alves are so large that valve placed in riser will be too high to reach

In these cases, offsets should be made in piping and should be done as shown in the examples of Figures 4-22, 4-23, and 4-24. Note that the offsets are made toward the allotted piping space, and not back over the pump.



GOOD USE WHEN DISCHARGE CHECK AND GATE **CAN BE** FLANGED TOGETHER

Figure 4-2-2.

The basic considerations for piping turbines are much like those for pumps. Unfortunately, most turbines have side connections, but we can, in most cases, at least specify right- or left-hand exhaust connections. This means that we have an initial choice of whether or not to have inlet and exhaust on the same side of the turbine. What governs the decision? The complexity of the piping. If the piping is

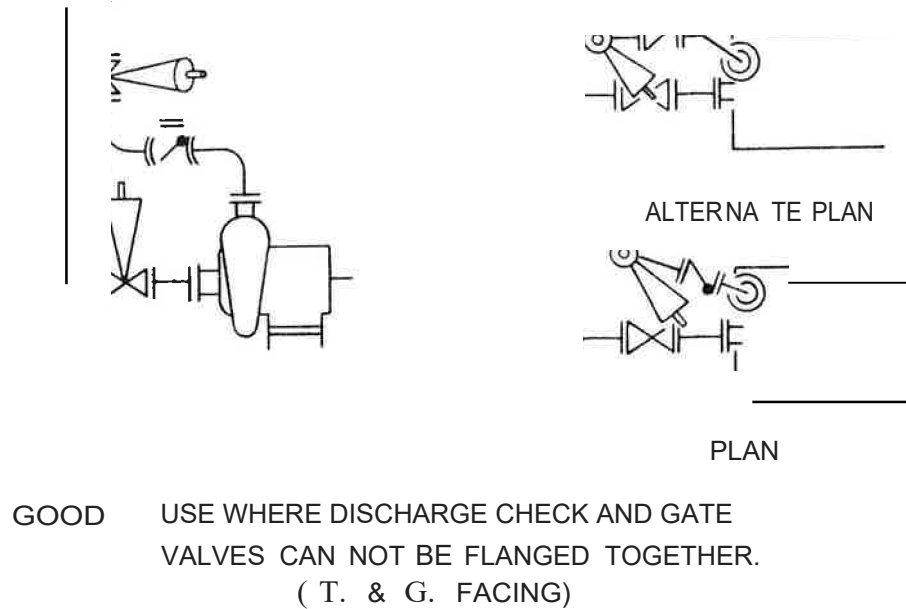


Figure 4-23.

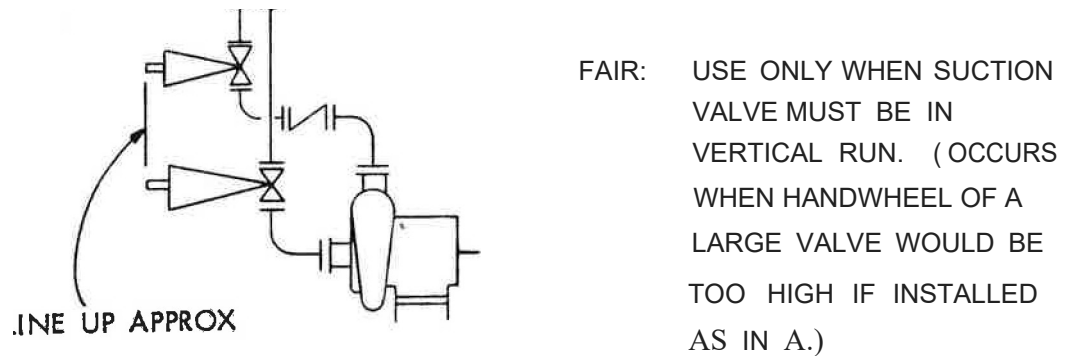


Figure 4-24.

simple ("inlet valve; exhaust valve; no relief valve), it will be best to have connections on the same side. If an APS is involved, a simple study should be made to see if both connections can be on the same side.

Let's look at steam piping to a turbine (Figure 4-25):

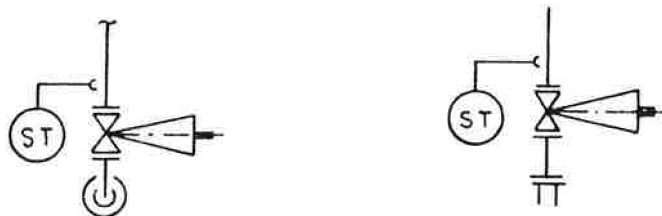


Figure 4-25.

These examples appear simple and, at a glance, reasonable, but this piping will be right alongside the turbine, the valve stem protrudes, the trap or blowdown valve will not completely drain the inlet piping, and there is no suitable location for a support.

Correcting these faults, we have Figure 4-26:

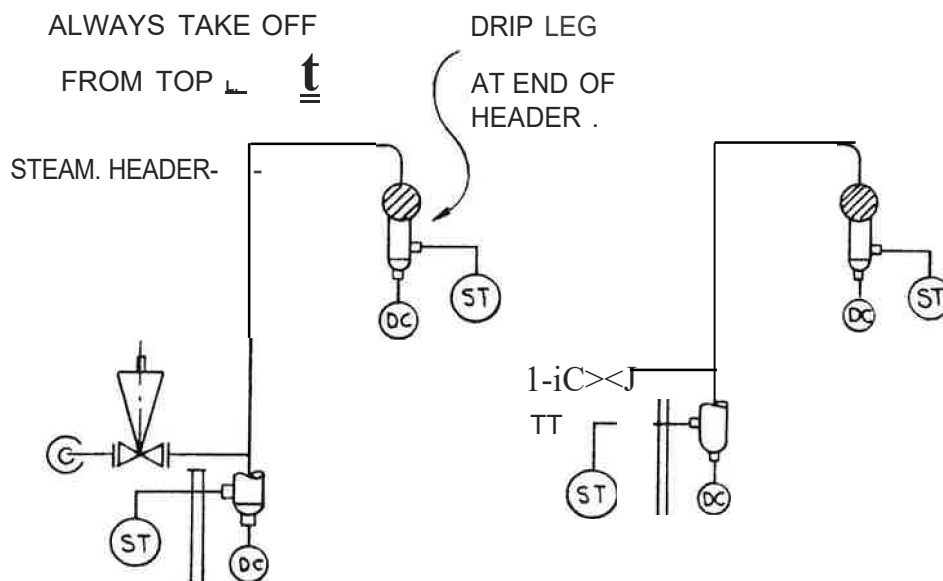


Figure 4-26 .

The good features we find here also apply to APS installations for single stage turbines (Figure 4-27):

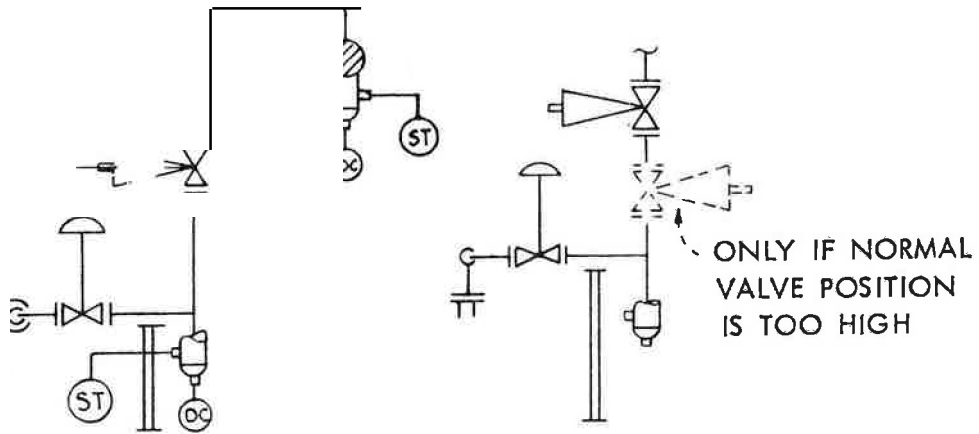


Figure 4-27.

These are good basic patterns for single stage turbines.

In the case of multi-stage steam turbines it is even more important to prevent carry-over of condensate. Water slugging will result in failure of the thrust bearings.

To accomplish this end, piping must have the following features:

(see Figure 4-28.)

1. Steam header must have at its termination a drip leg for continuous removal of condensate
2. Vertical steam line to turbine must have:
 - a) A dial thermometer located at least one pipe diameter below branch to turbine, to indicate presence of water

- b) A steam trap take-off below the sensing element of the dial thermometer
- c) A two-inch minimum blow-down valve, easily accessible, to allow complete removal of condensate to an exhaust stack located far enough from valve for safe operation

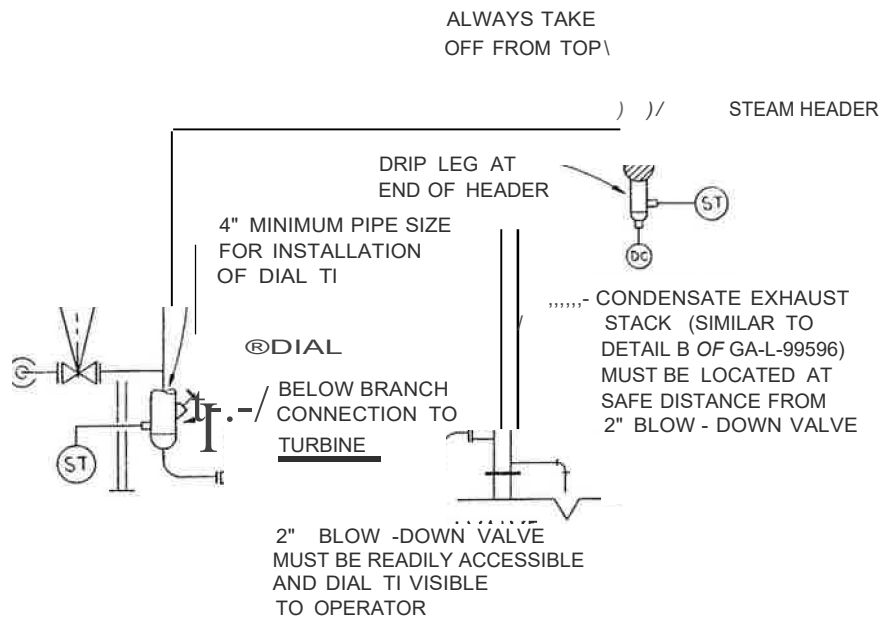


Figure 4-28.

What about exhaust piping? The problem is a bit different.

We need not worry about drainage as much, since the exhaust valve will usually stand open and drain the line through the case trap. This also keeps the case warm, avoiding thermal shock on startup.

The simplest choice may be appropriate (Figure 4-29), but if there is a support or anchor problem, or if the valve stem will project in an unsafe manner, we should consider

the arrangement of Figure 4-30. This arrangement is also advisable in cases where a relief valve is involved (Figure 4-31).

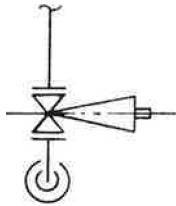


Figure 4-29.

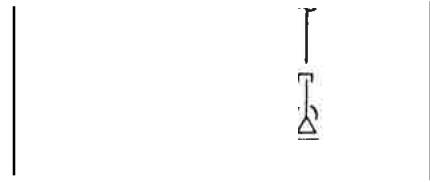


Figure 4-30.

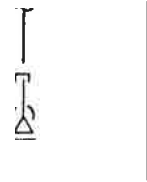


Figure 4-31.

In placing any of the above recommended piping around a turbine, keep in mind the problem of access to packing glands, lube oil connections, and the governor. A plan view of a proper piping arrangement might look like Figure 4-32 or, alternatively, Figure 4-33.

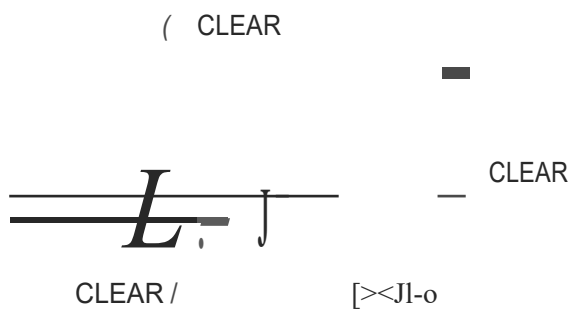


Figure 4-32.

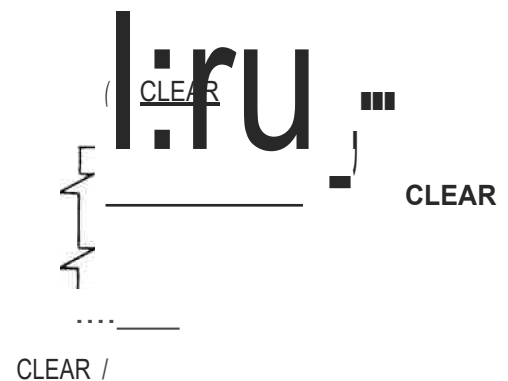


Figure 4-33.

-L 6 EXAMPLES OF PIPING ARRANGEMENTS

Drawings 21 E - L - 1 02 and 21 E - L - 7 3 show typical piping arrangements at centrifugal pumps for off-site locat io n.

Figures 4-34, 4-35, 4-36, and 4-37 are photographs of scale models and show typical piping a r a n g e m e n t s at centrifugal pumps for on-site location.

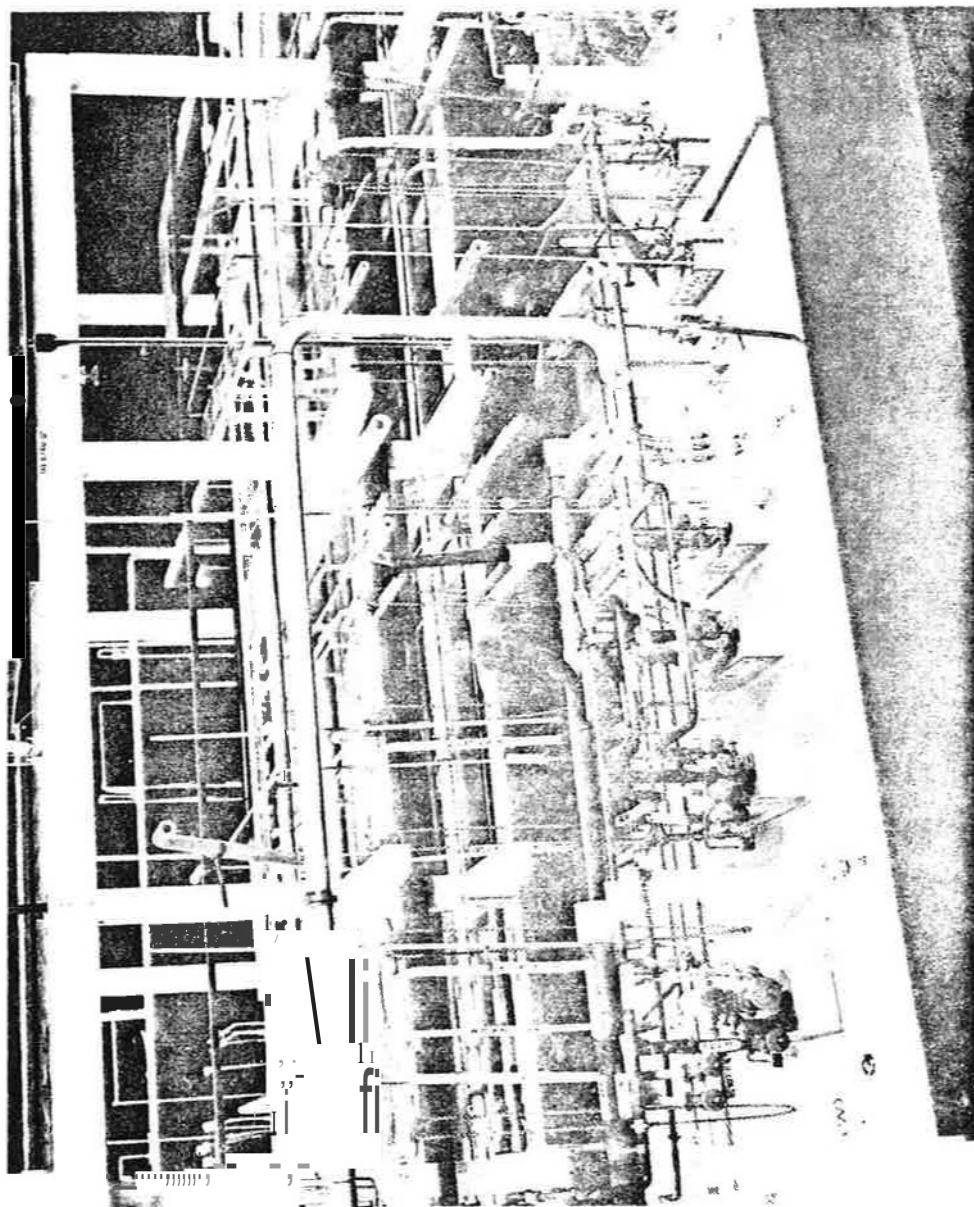


Figure 4-34

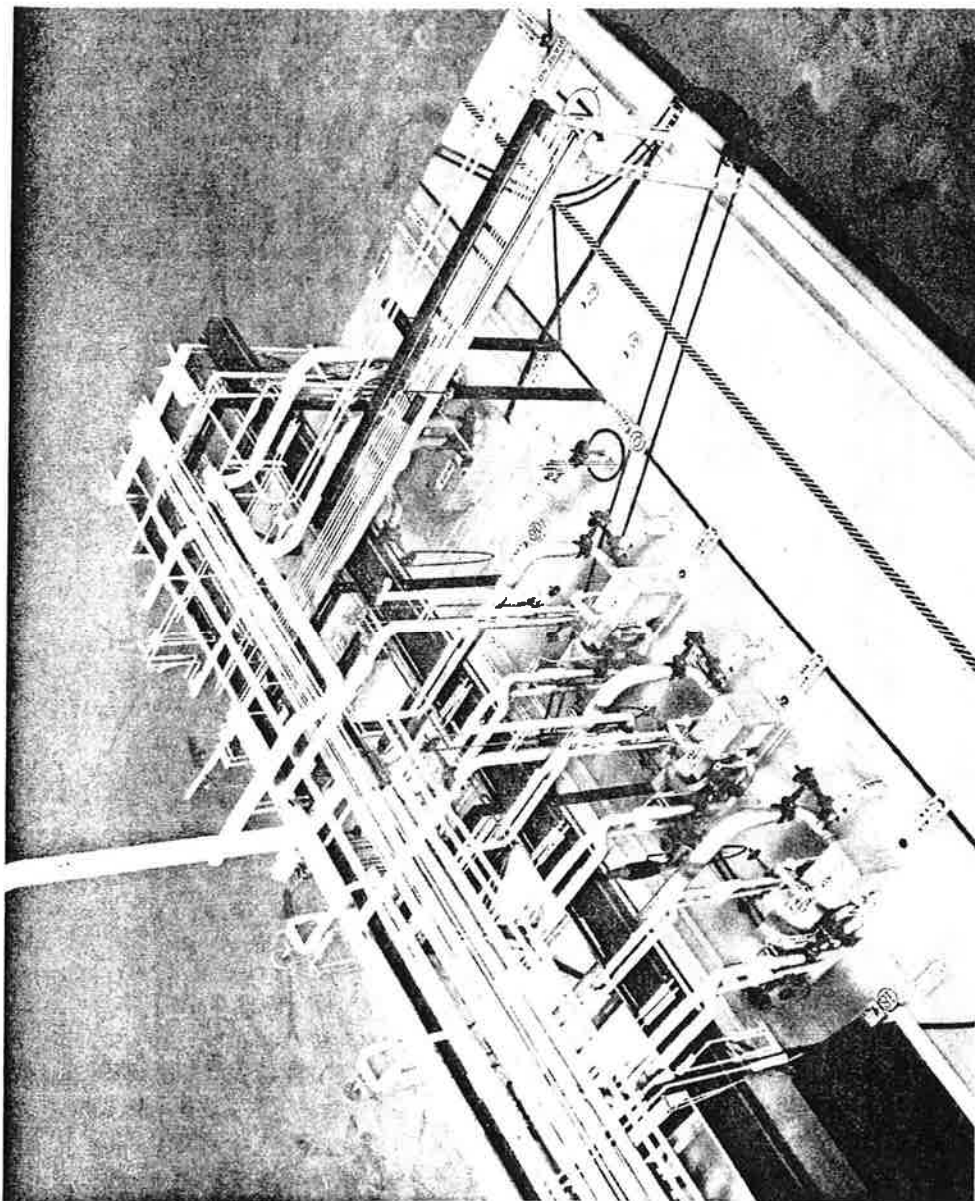


Figure 4-35.

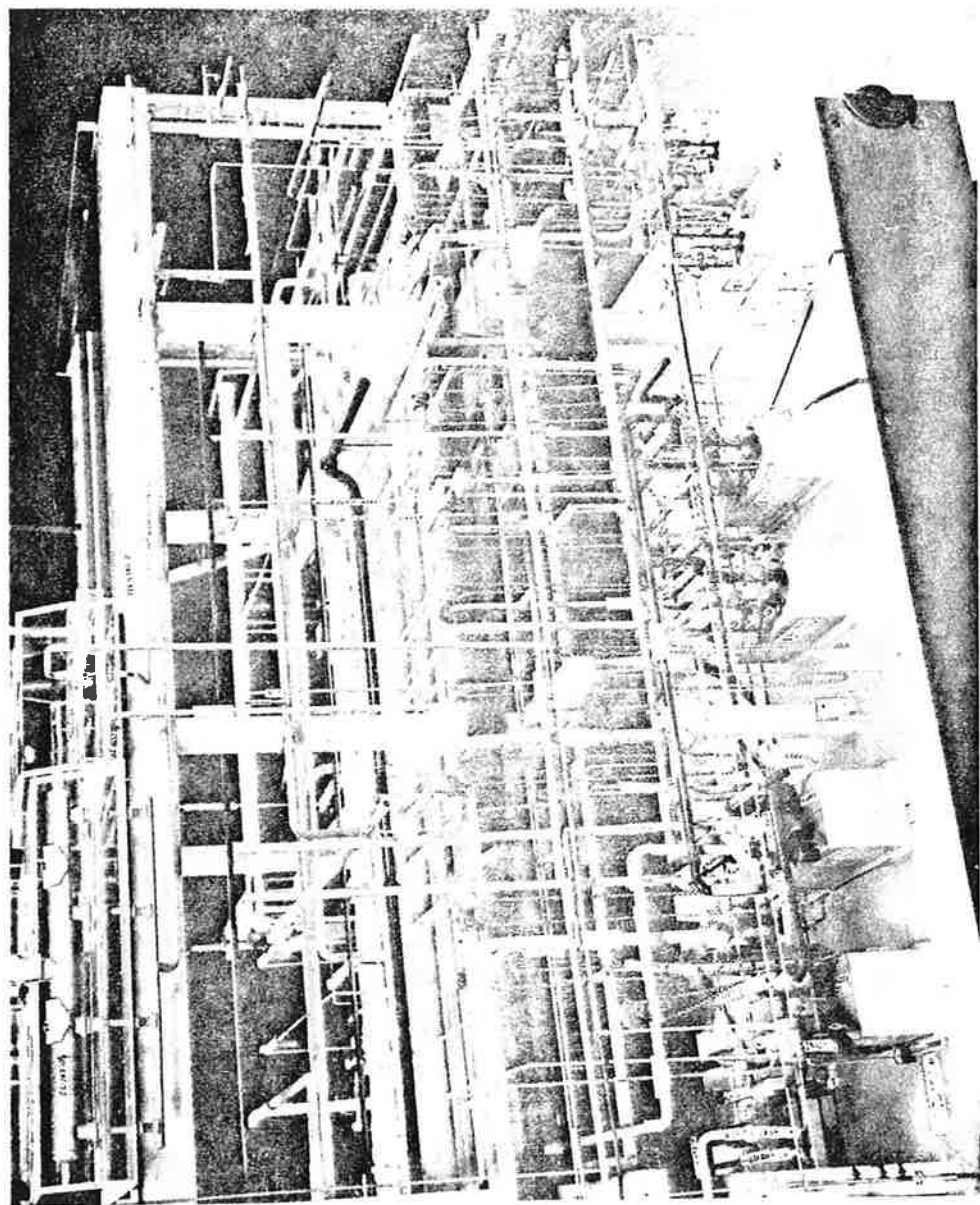


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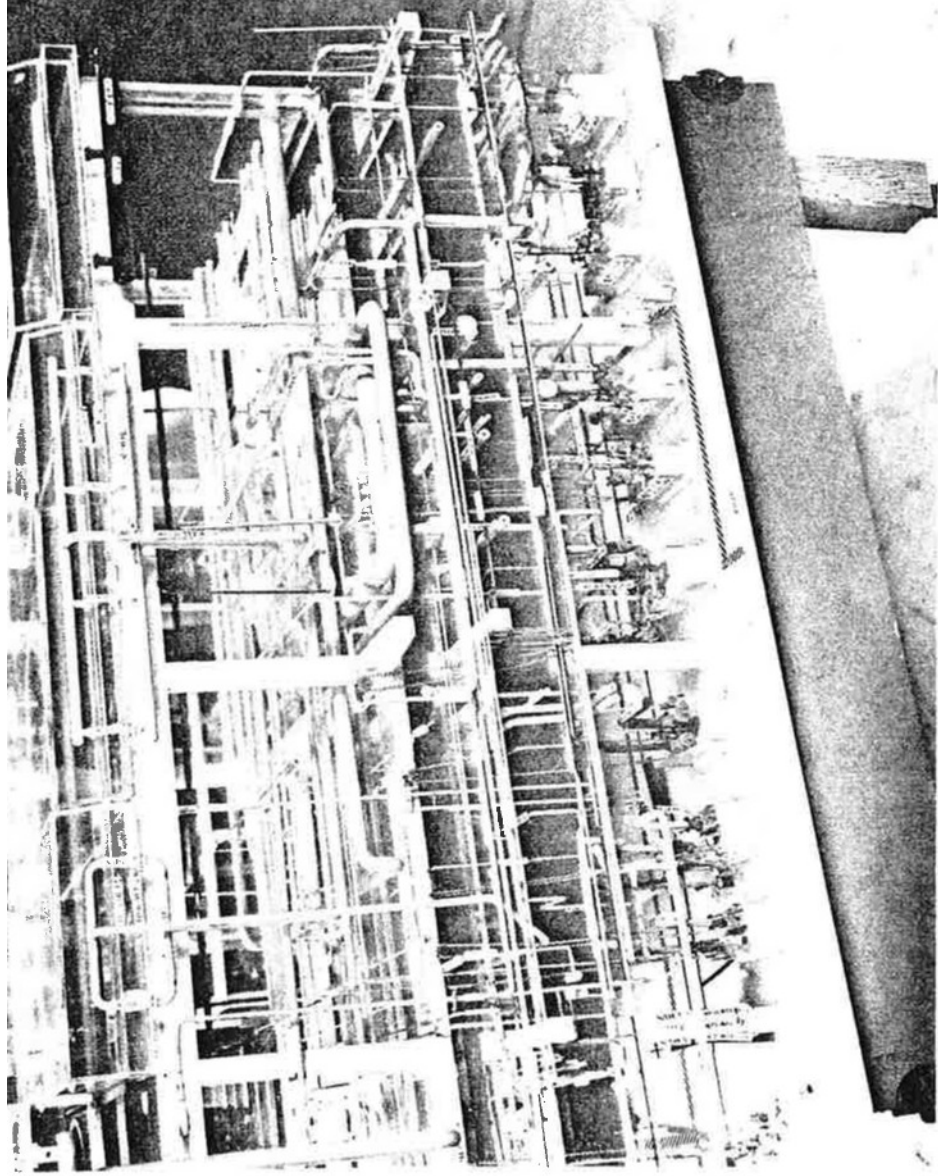
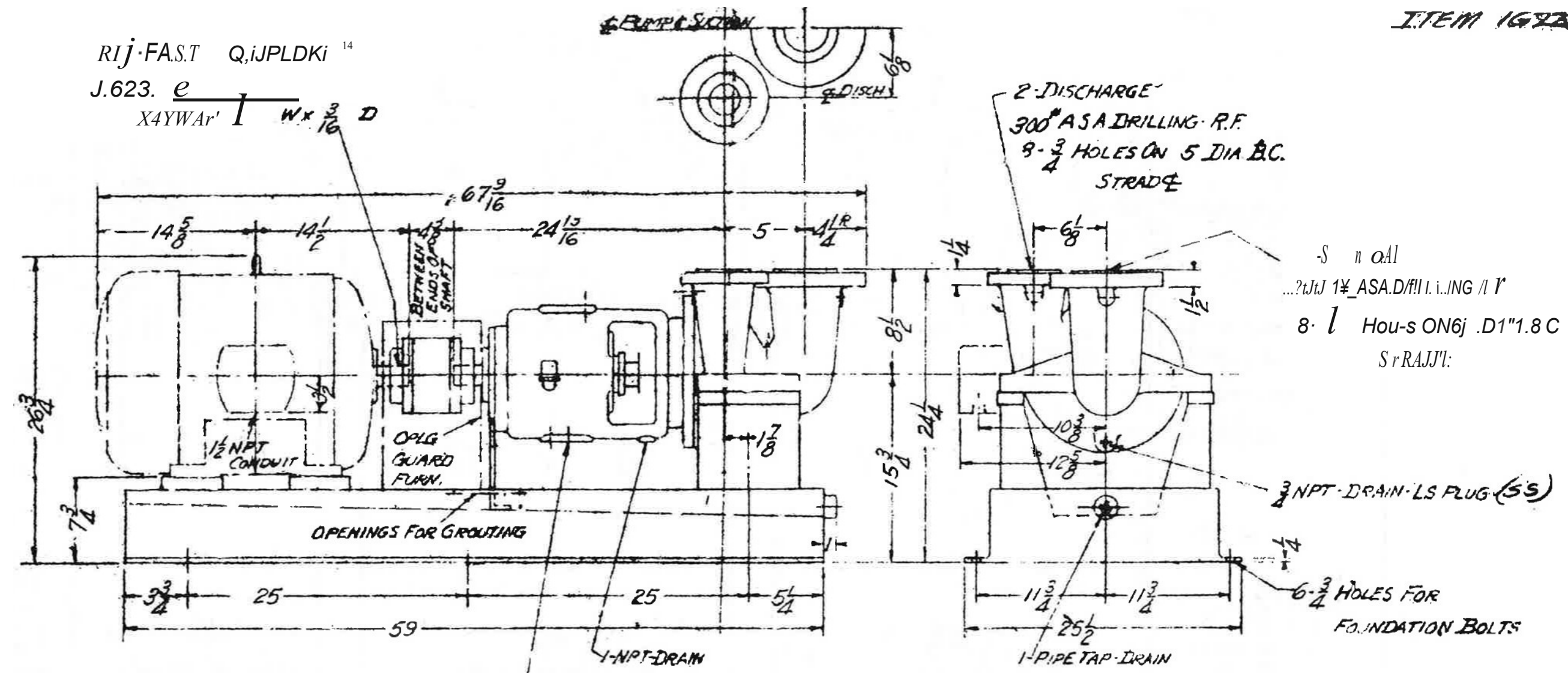


Figure 4-37.



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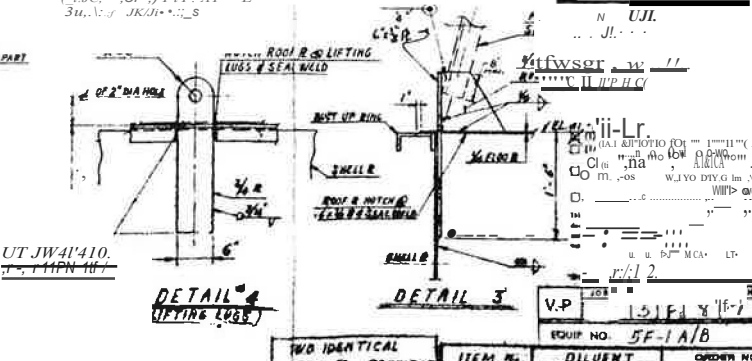
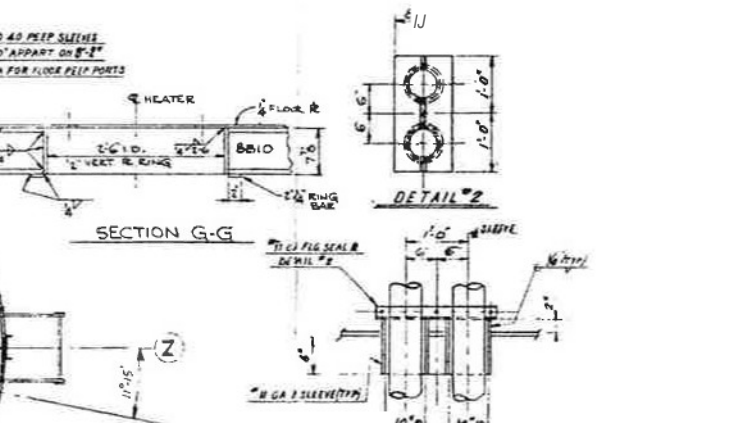
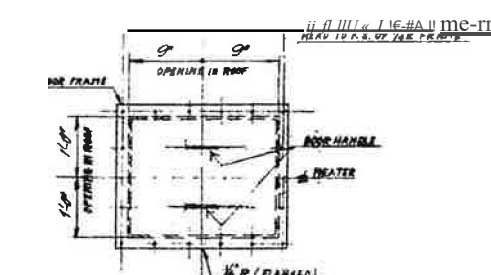
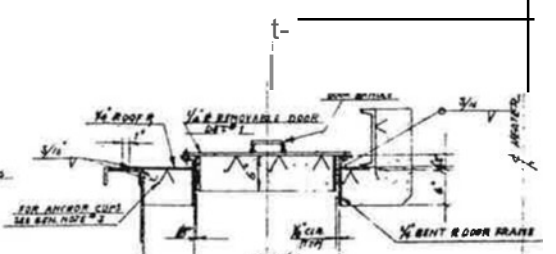
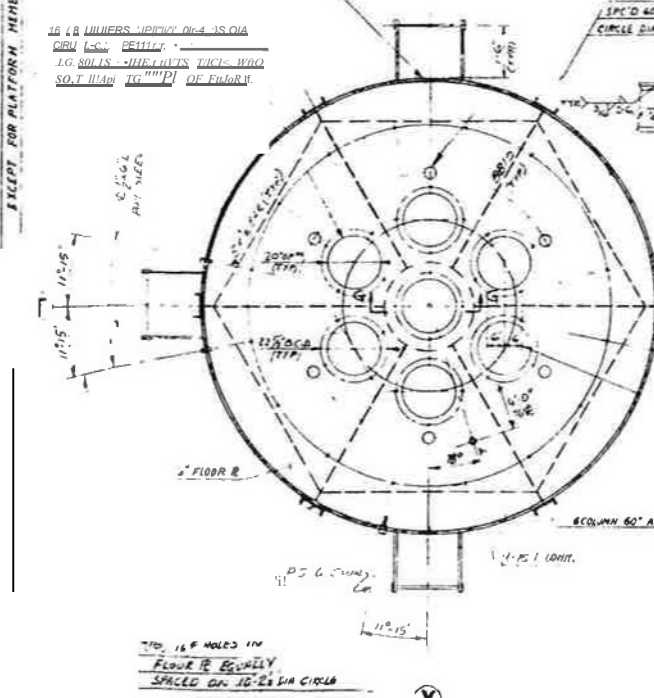
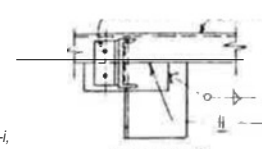
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B	7-5-65	ORDER OF SUBCONTRACTOR SEC. 2 - L.V.N.T.H.
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LETTER	DATE	DESCRIPTION
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	4-2-65	SELECTION STAR MARK
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		② FABRICATION
		③ PREPARATION OF SHOP DETAILS
		④ CUSTOMER COMMENTS
		⑤ PURCHASE OF ALL MATERIALS

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